## ON THE SOLUTION OF NONSTATIONARY HEAT-CONDUCTION PROBLEMS WITH VARIABLE HEAT-TRANSFER COEFFICIENT

V. N. Kozlov UDC 536.21

The article describes an exact method for calculating the temperature field in solids when they are heated in a medium with a variable heat-transfer coefficient and a nonuniform initial temperature distribution.

In [1] a method for the exact calculation of the temperature field of a solid object undergoing heat exchange in a medium with a variable temperature and a variable heat-transfer coefficient was discussed for a large number of Bi(Fo) functions of practical interest, as applied to an infinite plate. For  $\theta(1, Fo)$ , the temperature of the heated surface, we found in [1] an ordinary differential equation with variable coefficients which is solvable by operational methods [2]. The initial temperature distribution was assumed to be zero. We shall now show, using the example of a plate, how to deal with a nonuniform initial distribution. We shall assume that the temperature of the medium is zero. Heat transfer takes place at the plate surface X = 1, while the surface X = 0 is thermally insulated.

To solve the problem, we must establish how  $\partial\Theta(1, Fo)/\partial X$  varies with  $\Theta(1, Fo)$ .

It was shown in [3] that if Fo > 0, the function  $\partial\Theta(1, Fo)/\partial X$  can be represented as a convergent series

$$\frac{\partial \Theta (1, \text{ Fo})}{\partial X} = \sum_{i=1}^{\infty} Z_i (\text{Fo}), \tag{1}$$

in which  $Z_i(Fo)$ ,  $i = 1, 2, \ldots$ , are determined from the solution of the ordinary differential equations

$$T_i \dot{Z}_i$$
 (Fo)  $+ Z_i$  (Fo)  $= 2T_i \dot{\Theta}(1, \text{ Fo}), i = 1, 2, ...,$  (2)

with initial conditions  $Z_i(0) = Z_i^0$ , uniquely determined by the initial temperature distribution function. For the equations in (2) we have

$$T_i = \frac{4}{(2i-1)^2 \pi^2}.$$

The solutions  $Z_i$  (Fo) of these equations with initial conditions  $Z_i^{\theta}$  which are nonzero at time Fo = 0-0 (before the start of the perturbation) will be identical for Fo  $\geq$  0 + 0 (after the start of the perturbation) with the solutions  $y_i$  (Fo) of the equations

$$T_i \dot{y}_i (\text{Fo}) + y_i (\text{Fo}) = 2T_i \dot{\Theta} (1, \text{Fo}) + T_i Z_i^0 \delta (\text{Fo}), i = 1, 2, ...,$$
 (3)

with initial conditions which are zero at time Fo = 0-0 [4]. Here  $\delta$ (Fo) is the Dirac  $\delta$ -function.

Summation of the left and right sides of Eq. (3), taking account of (1) and the identities  $Z_i$  (Fo)  $\equiv y_i$  (Fo), which are valid for Fo  $\geq 0 + 0$ , yields:

$$-\sum_{i=1}^{\infty} T_i \dot{y}_i \text{(Fo)} + \dot{\Theta} \text{(1, Fo)} \sum_{i=1}^{\infty} 2T_i = \frac{\partial \Theta \text{(1, Fo)}}{\partial X} - \delta \text{(Fo)} \sum_{i=1}^{\infty} T_i Z_i^0.$$
(4)

Now we multiply each equation of (3) by T; and differentiate term by term:

$$T_i^2 \ddot{y}_i \text{ (Fo)} + T_i \dot{y}_i \text{ (Fo)} = 2T_i^2 \ddot{\Theta} (1, \text{ Fo)} + T_i^2 Z_i^0 \dot{\delta} \text{ (Fo)}, i = 1, 2, \dots$$
 (5)

F. E. Dzerzhinskii Heat Engineering Institute, Moscow. Translated from Inzhenerno-Fizicheskii Zhurnal, Vol. 20, No. 5, pp. 921-924, May, 1971. Original article submitted March 25, 1970.

© 1973 Consultants Bureau, a division of Plenum Publishing Corporation, 227 West 17th Street, New York, N. Y. 10011. All rights reserved. This article cannot be reproduced for any purpose whatsoever without permission of the publisher. A copy of this article is available from the publisher for \$15.00.

Summing with respect to i in (5), we obtain the sum  $\sum_{i=1}^{\infty} T_i \dot{y}_i$  (Fo) and substitute the resulting expression into (4):

$$\sum_{i=1}^{\infty} T_i^2 \ddot{y_i} (\text{Fo}) - \ddot{\Theta} (1, \text{ Fo}) \sum_{i=1}^{\infty} 2T_i^2 + \dot{\Theta} (1, \text{ Fo}) \sum_{i=1}^{\infty} 2T_i = \frac{\partial \Theta (1, \text{ Fo})}{\partial X} - \delta (\text{Fo}) \sum_{i=1}^{\infty} T_i Z_i^0 + \dot{\delta} (\text{Fo}) \sum_{i=1}^{\infty} T_i^2 Z_i^0.$$
 (6)

Proceeding with repeated transformations of this kind we finally obtain an ordinary differential equation for  $\Theta(1, F_0)$ :

$$\sum_{n=1}^{\infty} a_n \frac{d^n}{dFo^n} \Theta(1, Fo) = \frac{\partial \Theta(1, Fo)}{\partial X} + \sum_{m=0}^{\infty} b_m \frac{d^m}{dFo^m} \delta(Fo)$$
 (7)

with the coefficients

$$a_n = (-1)^{n+1} \sum_{i=1}^{\infty} 2T_i^n, \ n = 1, 2, \dots$$
 (8)

$$b_m = (-1)^{m+1} \sum_{i=1}^{\infty} Z_i^0 T_i^{m+1}, \ m = 0, 1, \dots$$
 (9)

Taking account of the boundary condition of the third kind for the case of a medium at zero temperature,

$$-\frac{\partial\Theta(1, \text{ Fo})}{\partial X} = \text{Bi (Fo)}\,\Theta(1, \text{ Fo}),\tag{10}$$

we finally arrive at the equation

Bi (Fo) 
$$\Theta(1, \text{ Fo}) + \sum_{n=1}^{\infty} a_n \frac{d^n}{d\text{Fo}^n} \Theta(1, \text{ Fo}) = \sum_{m=0}^{\infty} b_m \frac{d^m}{d\text{Fo}^m} \delta(\text{Fo}).$$
 (11)

It follows from the method used for obtaining Eq. (11) that here the initial conditions for Fo = 0-0 will be zero.

Assume, as in [1], that

$$Bi(Fo) = Bi_0 - f_0(Fo),$$
 (12)

where  $Bi_0 = const$  and  $f_0(Fo)$  is representable by a rational combination of sines (or cosines), polynomials, and exponents.

Proceeding in a manner analogous to [1], for a solution of Eq. (11), in the image domain, we make use of the "bifrequency transfer function" method of [2]. According to [2],

$$\overline{\Theta}(1, s) = \underset{Fo \to s}{L} \Theta(1, Fo) = \sum_{q=q_i} \frac{1}{(\gamma_i - 1)!} \frac{d^{\nu_j - 1}}{dq^{\nu_j - 1}} [(q - q_j)^{\nu_j} W(s, q)], \tag{13}$$

where the sum is taken over all the  $q_j$ -poles of the second argument of the function W(s, q), and  $\nu_j$  is the multiplicity of these poles.

If (12) is satisfied, we can obtain the bifrequency transfer function W(s, p) in the form of the absolutely and uniformly convergent series

$$W(s, p) = \sum_{v=0}^{\infty} W_v(s, p).$$
 (14)

In the problem under consideration the zeroth term of this series yields the formula

$$W_0(s, p) = \frac{1}{p\Psi(s)} \sum_{k=0}^{\infty} b_k s^k, \tag{15}$$

where

$$\Psi(s) = \text{Bi}_0 + \sum_{k=1}^{\infty} a_k s^k, \tag{16}$$

and the  $a_k$  and  $b_k$  are the coefficients (8) and (9) of Eq. (11).

It should be noted that the sum in (16) is a series expansion of the function  $\sqrt{s}$  th  $\sqrt{s}$ , and in (15)

$$\sum_{k=0}^{\infty} b_k s^k = -\sum_{i=0}^{\infty} \frac{Z_i^0}{s + \frac{1}{T_i}}.$$
 (17)

Therefore

$$W_0(s, p) = -\frac{1}{p\Psi(s)} \sum_{i=0}^{\infty} \frac{Z_i^0}{s + \frac{1}{T_i}},$$
(18)

$$\Psi(s) = \text{Bi}_0 + \sqrt{s} \, \text{th} \, \sqrt{s}. \tag{19}$$

All the subsequent  $(\nu = 1, 2, ...)$  terms of the series (14) are found by the recursion formula:

$$W_{\mathbf{v}}(s, p) = \sum_{q=q_j} \frac{1}{(v_j - 1)!} \frac{d^{v_j - 1}}{dq^{v_j - 1}} \left[ (q - q_j)^{v_j} W_u(s, q) W_{\mathbf{v} - 1}(s - q, p - q) \right]. \tag{20}$$

The sum in (20) is taken over all the  $q_i$ -poles of multiplicity  $\nu_i$  of the second argument of the bifrequency transfer function  $W_{ij}(s,q)$ , which in our problem has the form

$$W_u(s, q) = \frac{F_0(q)}{\Psi(s)}, \ F_0(q) = \underset{F_0 \to q}{L} f_0(F_0).$$
 (21)

After determining the temperature  $\Theta(1, Fo)$ , the temperature field of the plate  $\Theta(X, Fo)$  can be found from the solution of the problem with a boundary condition of the first kind.

## NOTATION

| Θ                              | is the temperature;               |
|--------------------------------|-----------------------------------|
| L                              | is the thickness of plate;        |
| X                              | is the space coordinate;          |
| a                              | is the thermal diffusivity;       |
| λ                              | is the thermal conductivity;      |
| α                              | is the heat-transfer coefficient; |
| t                              | is the time;                      |
| X = x/L                        | is the dimensionless coordinate;  |
| $Fo = at/L^2$                  | is the Fourier number;            |
| $Bi(Fo) = \alpha(Fo)L/\lambda$ | is the Biot number.               |

## LITERATURE CITED

- 1. V. N. Kozlov, Inzh. Fiz. Zh., 18, 1 (1970).
- 2. I. N. Brikker, Avtomat. i Telemekhan., 8 (1966).
- 3. V. N. Kozlov, Inzh. Fiz. Zh., 15, No. 5 (1968).
- 4. A. V. Solodov, Linear Automatic-Control Systems with Variable Parameters [in Russian], Fizmatgiz (1962).